

PROJECT: Western Flyer Crane repair (Allied Sysetms crane)

ENGINEER: J.Erickson: M.Brown

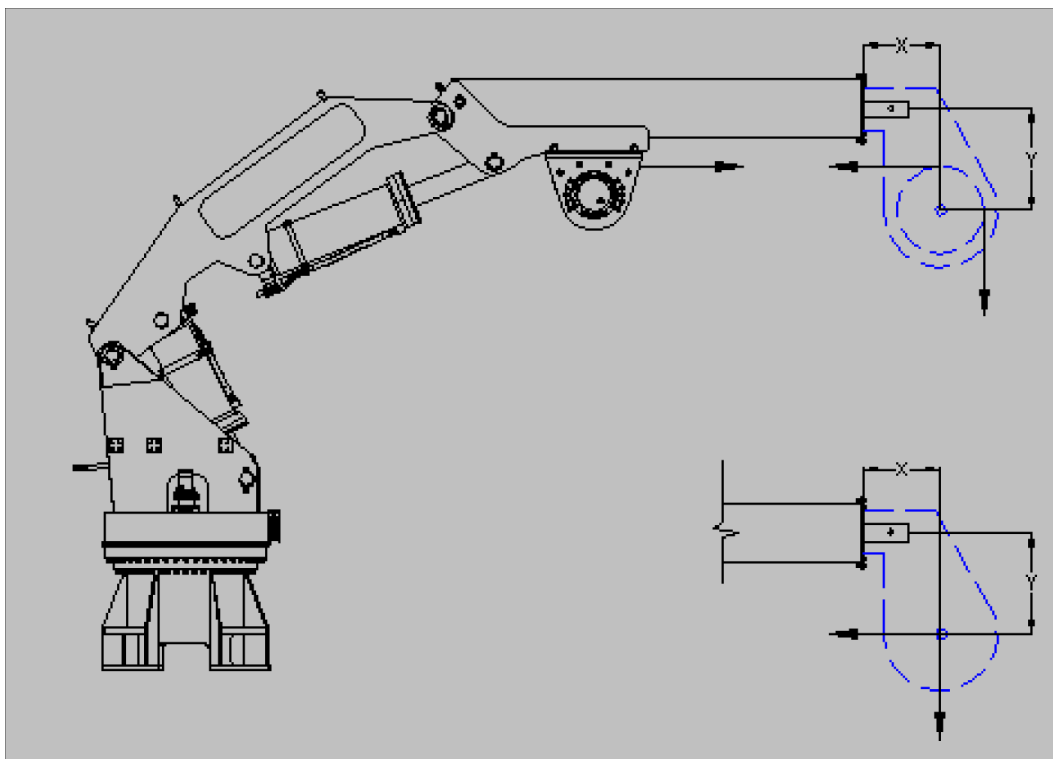
REFERENCE:

Roark's Formulas for Stress and Strain 6th edition

Mechanical Engineering Design: Shigley 5th ed.

Title: Static & Dynamic analysis

PROPERTIES & ASSUMPTIONS:



$X := 11.75 \cdot \text{in}$

$\text{HEAD_WEIGHT} := 2300 \cdot \text{lbf}$

$Y := 29 \cdot \text{in}$

$\text{LINE_TENSION} := 23780 \cdot \text{lbf}$

$$\text{MOMENT_FLANGE} := \text{LINE_TENSION} \cdot Y + (\text{LINE_TENSION} + \text{HEAD_WEIGHT}) \cdot X$$

$$\text{MOMENT_FLANGE} = 996060 \text{ in} \cdot \text{lbf}$$

$$b := 9 \cdot \text{in}$$

$$d := 12 \cdot \text{in}$$

$$\text{INERTIA_WELD} := (.375 \cdot \text{in}) \cdot (.707) \cdot \left[\frac{(12 \cdot \text{in})^2}{6} \cdot ((3 \cdot 9 \cdot \text{in} + 12 \cdot \text{in})) \right]$$

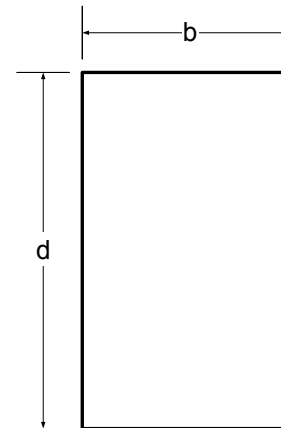
$$\text{INERTIA_WELD} = 248 \text{ in}^4$$

$$\text{WELD_STRESS} := \frac{\text{MOMENT_FLANGE} \cdot 6 \cdot \text{in}}{\text{INERTIA_WELD}}$$

$$\text{WELD_STRESS} = 24083 \text{ psi}$$

$$\text{FACTOR_OF_SAFETY_WELD} := \frac{70000 \cdot \text{psi}}{\text{WELD_STRESS}}$$

$$\text{FACTOR_OF_SAFETY_WELD} = 2.91$$



Boom extension
Rectangular Tube

For each Gusset, compute the Inertia:

$$\text{INERTIA_GUSSET} := \frac{.707 \cdot .375 \cdot \text{in} \cdot (1.75 \cdot \text{in})^3}{12}$$

$$\text{INERTIA_GUSSET} = 0.118409 \text{ in}^4$$

$$\text{Area_GUSSET} := .707 \cdot .375 \cdot \text{in} \cdot 1.75 \cdot \text{in}$$

$$\text{Area_GUSSET} = 0.464 \text{ in}^2$$

$$d := 6.875 \cdot \text{in}$$

parallel Axis Th.

$$I' := \text{INERTIA_GUSSET} + (\text{Area_GUSSET} \cdot d^2)$$

$$I' = 22.048 \text{ in}^4$$

For 4ea Gussets there are 8 welds. Therefore the total Inertia of the Gussets is:

$$\text{GUSSET_INERTIA}_T := 8 \cdot I'$$

$$\text{GUSSET_INERTIA}_T = 176.385 \text{ in}^4$$

2/6/2009

$$\text{Total_Weld_Inertia} := \text{INERTIA_WELD} + \text{GUSSET_INERTIA}_T$$

$$\text{Total_Weld_Inertia} = 424.542 \text{ in}^4$$

Maximum Weld Stress @ end of Gusset:

$$\text{Total_Weld_Stress} := \frac{\text{MOMENT_FLANGE} \cdot 7.75 \cdot \text{in}}{\text{Total_Weld_Inertia}}$$

$$\text{Total_Weld_Stress} = 1.818 \times 10^4 \text{ psi}$$

$$\text{Total_FS_Weld} := \frac{70000 \cdot \text{psi}}{\text{Total_Weld_Stress}}$$

$$\text{Total_FS_Weld} = 3.85$$

Looks like we can't get over 4 here
but we feel there is plenty of safety
factor anyhow.

Below: Jon took a look at trying to plug weld to the existing verticals to see if we gained anything
(not much)

Calc Inertia for each Plug Weld:

$$\text{INERTIA_PLUG_WELD} := \frac{.707 \cdot .375 \cdot \text{in} \cdot (.750 \cdot \text{in})^3}{12}$$

$$\text{INERTIA_PLUG_WELD} = 9.321 \times 10^{-3} \text{ in}^4$$

$$\text{Area_Plug_Weld} := .707 \cdot .375 \cdot \text{in} \cdot .75 \cdot \text{in}$$

$$\text{Area_Plug_Weld} = 0.199 \text{ in}^2$$

$$\text{dd} := 5.375 \cdot \text{in}$$

parallel axis th.

$$I_{pw} := \text{INERTIA_PLUG_WELD} + (\text{Area_Plug_Weld} \cdot \text{dd}^2)$$

$$I_{pw} = 5.754 \text{ in}^4$$

For 4 plug welds there are 8 weld sides:

$$\text{PW_INERTIA}_T := 8 \cdot I_{pw}$$

$$\text{PW_INERTIA}_T = 46.032 \text{ in}^4$$