

# ESP MOORING WHOT CABLE MODEL

## BUGY

mass = 34 kg (75 lbs)

Axisymmetric

| $\bar{z}$ | $d$ |
|-----------|-----|
| 0         | 3"  |
| 33"       | 3"  |
| 33"       | 11" |
| 42"       | 16" |
| 69"       | 16" |

$$S_w = .15 m^2$$

$$C_{dw} = 0.75$$

$$C_{dw} = 1.0$$

$$C_k = 0.1$$

## ESP ASSEMBLY

THERE ISN'T A GREAT WAY TO MODEL THIS RAIL ARRANGEMENT IN WHOT CABLE. TWO APPROACHES ARE USED:

A) SIMPLEST, AND WRONG B/C IT DOESN'T INCLUDE THE RAIL HINGED DOWN LOW

→ MODELED AS A CYLINDER OF APPROPRIATE SIZE WITH A MOMENT RELEASING CONNECTOR AT THE TOP AND BOTTOM.

$$m = 386 \text{ kg (850 lbs)} \quad [193 \text{ kg/m}]$$

$$\text{WET WEIGHT} = -890 \text{ N (-200 lbs)} \quad [-445 \text{ N/m}]$$

$$d = .762 \text{ m (30")}$$

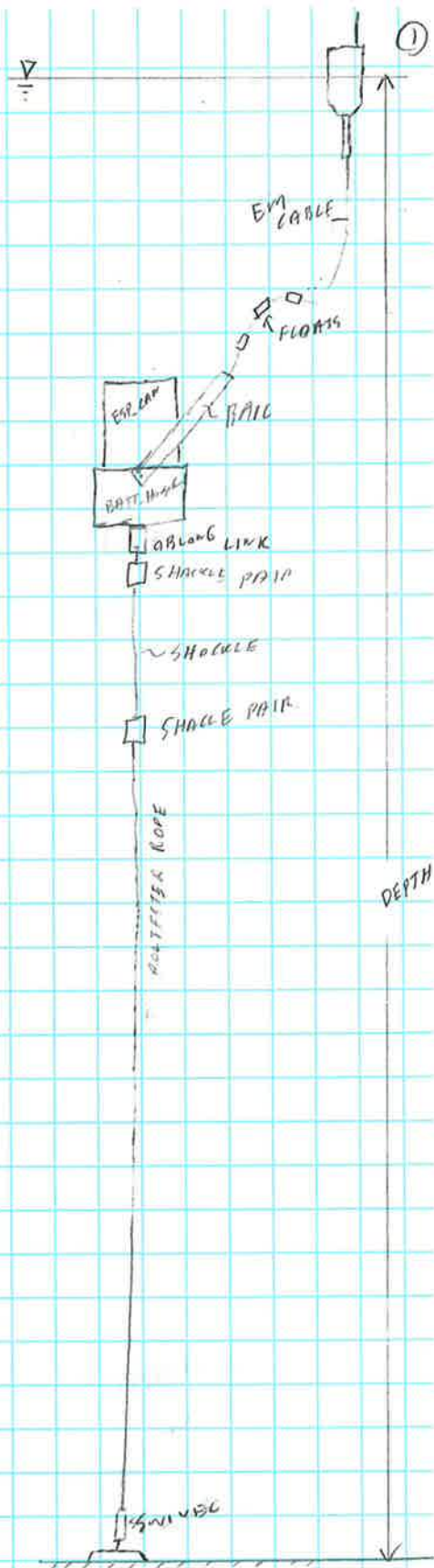
$$L = 2.0 \text{ m (79")}$$

$$C_d = 1.0 \quad C_{an} = 1.0$$

$$C_L = 1.0 \quad C_{aL} = 1.0$$

B) MORE COMPLICATED, MODEL ASSEMBLY AS

THREE COMPONENTS, BATTERY CASE RAIL CONNECTED TO TOP OF BATTERY CASE, WITH A MOMENT RELEASING CONNECTOR, AND ESP AS "ATTACHMENTS" ADDING DRAG/MASS/WET-WEIGHT TO TOP NODE OF BATTERY CASE. SUM OF THE MASS AND WEIGHT OF THE THREE ELEMENTS SUM TO THE APPROPRIATE TOTAL VALUE.





## B (cand)

### BATTERY CASE

$$EA = 1e7 \quad EI = 5e5$$

$$m = 120 \text{ kg} \quad 181.8 \text{ kg/m}$$

$$264 \text{ lbs}$$

$$\text{WET WEIGHT} = 647 \text{ N} \quad 980 \text{ N/m}$$

$$145 \text{ lbs}$$

### BAIL

$$EA = 1e7 \quad EI = 1.4e4$$

$$m = 30.4 \text{ kg} \quad 22.9 \text{ kg/m}$$

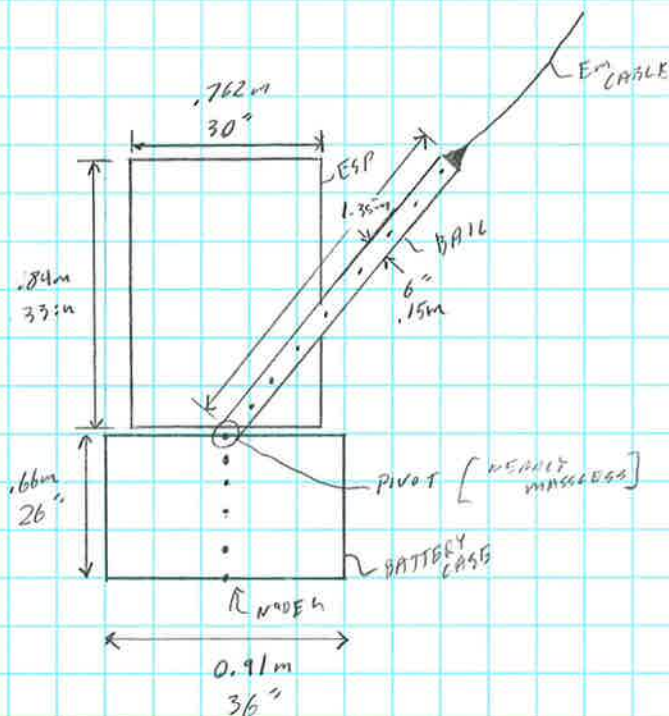
$$68 \text{ lbs}$$

$$\text{WET WEIGHT} = 0 \text{ N} \quad 0 \text{ lbs} \quad \left\{ \begin{array}{l} \text{CONSIDER IT} \\ \text{NEUTRAL} \end{array} \right.$$

### ESPCAN

$$m = 235 \text{ kg} = 517 \text{ lbs}$$

$$\text{WET WEIGHT} = -1540 \text{ N} = -346 \text{ lbs}$$



### Sum 5

$$m = 120 \text{ kg} + 30.4 \text{ kg} + 215 \text{ kg} = 386 \text{ kg} = 849 \text{ lbs}$$

$$\text{WET WEIGHT} =$$

## POLYESTER ROPE

$$EA = 1 \times 10^6 \text{ N} \quad [\text{FROM SPEC SHEET THAT INDICATES 1.1\% ELONGATION @ 2540 lbs}]$$

$$EI = 31 \text{ N} \cdot \text{m}^2 \quad [\text{EQUIVALENT ROD}]$$

$$d = .022 \text{ m} \quad [7/8 \text{ inch}]$$

$$m = .403 \text{ kg/m}$$

$$\text{wet weight} = 1.53 \text{ N/m} \quad [\text{FROM SPECIFIC GRAVITY} = 1.38 \text{ SPEC}]$$

## ROCHESTER EM CABLE

$$EA = 3.226 \times 10^6 \text{ N} \quad [\text{FROM SPEC SHEET}]$$

$$EI = 18 \text{ N} \cdot \text{m}^2 \quad [\text{EQUIVALENT ROD}]$$

$$d = .0096 \text{ m}$$

$$m = .370 \text{ kg/m}$$

$$\text{wet weight} = 2.97 \text{ N/m} \quad [\text{FROM SPEC SHEET, ADJUSTED FOR SEAWATER}]$$



# SYNTACTIC FLOATS - MODELLED AS CYLINDERS

$$d = .0762 \text{ m} [3"]$$

$$l_{\text{en}}, l_h = .1016 \text{ m} [4"]$$

$$m = .230 \text{ kg} [\text{MEASURED FROM SAMPLE}]$$

$$\text{wt. weight} = -2.17 \text{ N} [\text{COMPUTED FROM MEASURED MASS AND COMPUTED VOLUME}]$$

## SHACKLE

$$\rightarrow \begin{array}{l} 3 \text{ m LONG} \\ 5 \text{ m LONG @ } 200 \text{ lbs } [DL = 2 \text{ m}] \\ @ 7 \text{ m LIMITED TAXES OVER } [DL = 4 \text{ m}] \end{array}$$

### LINEAR OPTION:

$$m = .909 \text{ kg/m} [6 \text{ LBS FOR } 3 \text{ m LENGTH}]$$

$$d = .052 \text{ m} [\sim 2" \text{ DIAM}]$$

$$EA = 1335 \text{ N} [200 \text{ LBS STRETCHES } 3 \text{ m LENGTH TO } 5 \text{ m}]$$

$$EI = .226 \text{ N}\cdot\text{m}^2 [\text{BASED ON ROD EQUIVALENT, NOT A GREAT ASSUMPTION...}]$$

$$\text{wt weight} = 0 [\text{NEUTRAL}]$$

### NON-LINEAR OPTION $\rightarrow$ LOCUS

$$m = .909 \text{ kg/m} [6 \text{ LBS FOR } 3 \text{ m LENGTH}]$$

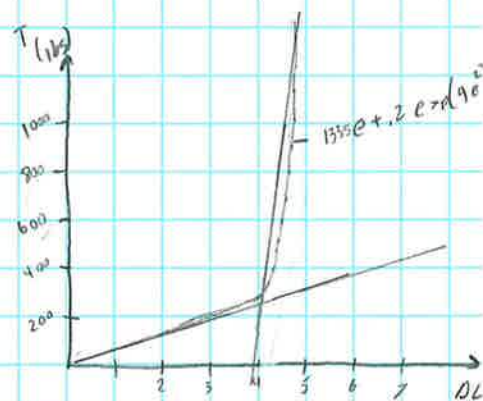
$$d = .052 \text{ m} [\sim 2" \text{ DIAM}]$$

$$\text{wt. weight} = 0$$

$$T(e) = 1335e + .2 \exp(4e^2) \leftarrow \text{SIMULATE SPECTRA STIFFNESS}$$

$$T'(e) = 1335 + .16 \exp(4e^2) \quad \text{ABOVE } 5 \text{ m LENGTH}$$

$$\begin{aligned} T''(e) &= (.16e)^2 \exp(4e^2) + .16 \exp(4e^2) \\ &= .16[.16e^2 + 1] \exp(4e^2) \end{aligned}$$



## SWIVEL AT ANCHOR

$$m = 5 \text{ kg} [9.43 \text{ kg/m}]$$

$$L = .53 \text{ m}$$

$$d = .0508 \text{ m} [2"]$$

$$\text{wt. weight} = 20 \text{ N} [37.7 \text{ N/m}]$$

## SHACKLE PAIR

$$m = 2 \text{ kg}$$

$$L \approx 0 \text{ } \frac{1}{2} \text{ connection}$$

$$\text{wt. weight} = 8 \text{ N}$$

## OBLONG LINK

$$m = 3 \text{ kg} [10 \text{ kg/m}]$$

$$L = .3 \text{ m}$$

$$\text{wt. weight} = 12 \text{ N} [40 \text{ N/m}]$$

POLYESTER ROPE (5/8")

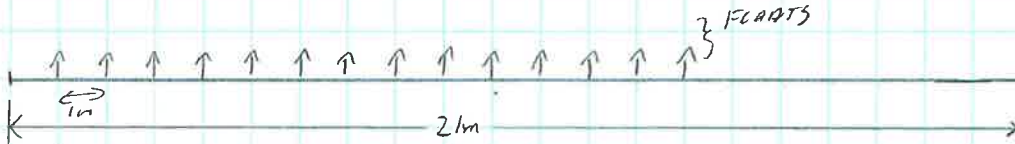
$$EA = 560,000 \text{ N} \text{ [SPEC SHEET INDICATES 11\% ELONGATION AT 1390 lbs]}$$

$$EI = 22 \text{ N}\cdot\text{m}^2 \text{ [EQUIV ROD]}$$

$$d = .0154 \text{ m} \text{ [5/8"]}$$

$$m = 0.14 \frac{\text{lbs}}{\text{ft}} \cdot \frac{1\text{ft}}{12\text{in}} \cdot \frac{1\text{in}}{.0254\text{m}} \cdot \frac{1\text{kg}}{2.2\text{lbs}} = 0.2088 \text{ kg/m}$$

$$\text{wet weight} = 0.778 \text{ N/m} \quad \left\{ \text{BASED ON T.G.} = 1.38 \right.$$

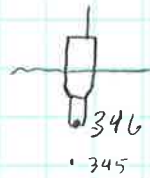
FM CABLE WITH FLOATS

$$\rightarrow \text{CABLE WET WEIGHT} = 2.97 \text{ N/m} = 62.4 \text{ N TOTAL}$$

$$\rightarrow \text{FLOAT WET WEIGHT} = -2.17 \text{ N/FLOAT} = 30.4 \text{ N TOTAL}$$

$$\rightarrow \text{MEAN WEIGHT OF FLOATED SECTION} = -0.8 \text{ N/m}$$





2 EM TETHER

- 307
- 306
- 305
- 304
- 303
- 302
- 301
- 300
- 299
- 298
- 297

BAIL

- PIVOT →
- 294
  - 293
  - 292
  - 291
  - 290
  - 289
  - 288
  - 287
  - 286

BATTERY CASE

- OBLONG LINK {
- 284
  - 283
  - 282
  - 281
  - 280
  - 279
  - 278
  - 277
  - 276
- SHACKLE PAIR
- SHOCKLE
- SHACKLE PAIR

POLYESTER ROPE

- 8
  - 7
  - 6
  - 5
  - 4
  - 3
  - 2
  - 1
- SHACKLE PAIR
- ANCHOR SWIVEL

